

PECENED: OTOS RORA **APPENDIX 12-3** 0> **BESS OPERATIONAL NOISE** REPORT



PRICEINED: OTOS ROZA

**Technical Appendix 12-3** 

# System (BESS) Noise Report Seskin Wind Farm, Co. Carlow

**EDF Renewables Ireland** 

01 May 2024

**COMMERCIAL IN CONFIDENCE** 



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### 1 Introduction

TNEI was commissioned by MKO on behalf of EDF Renewables Ireland Ltd to undertake a Noise Impact Assessment (NIA) for the operation of a Battery Energy Storage System (BESS) and associated plant, which forms part of the Proposed Seskin Wind Farm (hereinafter referred to as 'the Proposed Project').

The method of assessment of operational noise for a BESS is very different from that used for the assessment of operational wind turbine noise and the two assessment types cannot be combined. Accordingly, the assessment of operational noise attributable to the BESS is presented here in this report, and the operational wind farm noise assessment is provided in a separate report, Appendix 12-2.

The BESS is to be located within an area east of The Butts, at approximate ITM grid coordinates 663789, 669366. The land surrounding the proposed BESS is rural in nature, predominantly consisting of forested areas. A small number of residential properties are located within the area, the nearest of which is approximately 950m to the west and east.

The aims of this NIA are to:

- Identify the potential noise sensitive receptors in the vicinity of the proposed BESS;
- Identify the primary sound sources associated with the operation of the BESS;
- Calculate the likely levels of operational noise at the identified receptors to determine the noise impacts associated with the operation of plant within the BESS; and
- Indicate any requirements for mitigation measures, if required, to provide sufficient levels of protection for all noise sensitive receptors.

#### 1.1 Nomenclature

Please note the following terms and definitions, which are used throughout this report:

- **Emission** refers to the noise level emitted from a noise source, expressed as either a sound power level or a sound pressure level;
- **Immission** refers to the sound pressure level received at a specific location from a noise source;
- **SWL** indicates the sound power level in decibels (dB);
- **SPL** indicates the sound pressure level in decibels (dB);
- NML (Noise Monitoring Location) refers to any location where baseline noise levels have been measured;
- NSRs (Noise Sensitive Receptors) are all identified receptors which are sensitive to noise; and
- **BNAL** (BESS Noise Assessment Location) refers to any location where the noise immission levels are calculated and assessed.

A Glossary of Terms is also provided as Annex 1 of this report.

All figures referenced within the report can be found in Annex 5.

Unless otherwise stated, all sound levels refer to free field levels i.e. sound levels without influence from any nearby reflective surfaces.

All grid coordinates refer to the Irish Transverse Mercator (ITM) coordinate system using ITM X and ITM Y, unless stated otherwise.



# 2 Proposed Project Description

### 2.1 Description of the Proposed BESS Compound



The proposed BESS compound would introduce new sound sources to the local area in the form of externally located fixed plant. The BESS is expected to consist of a number of liquid cooled battery cubes, which would be connected into a series of Power Conversion Units (PCS), each consisting of a pair of inverters and a medium voltage (MV) transformer. It is also assumed that a High Voltage (HV) Grid Transformer will be located within an adjacent substation. Some auxiliary plant and switch gear may be associated with the operation of the HV transformer but would be insignificant in noise output in comparison to the HV transformer itself.

Specifically, the dominant sound sources considered within this assessment are assumed as follows:

- 64 x Fluence Cubes;
- 2 x Chint Electric MV Transformer;
- 4 x PE HEMK PCSK Inverter; and
- 1 x HV Grid Transformer

An indicative layout plan provides an overview of the proposed BESS in Annex 2.

### 2.2 Study Area

Noise Sensitive Receptors (NSRs) considered in this assessment are nearby residential properties. The study area for this assessment has been defined through the identification of the closest NSRs to the Proposed Project infrastructure . The closest NSR is located approximately 950 m to the west and with other receptors at similar or greater distances. Figure A5.1 in Annex 5 details location of the proposed BESS in context of the closest NSRs considered within the assessment.

The assessment of noise attributable to the proposed BESS considers the nearest NSRs only, on the assumption that if sound levels at the closest receptors are within the defined limits, then sound levels at NSRs at greater distances from the Proposed Project should also be within acceptable levels.



# 3 Assessment Methodology

### 3.1 Legislation and Policy Context

There is no published statutory Irish guidance which contains a detailed method for the assessment of industrial noise sources such as this proposed BESS. The assessment has therefore been undertaken following guidance from British Standard BS 4142 Method for rating and assessing industrial and BS 8233 Guidance on sound insulation and noise reduction for buildings.

### 3.2 Assessment Methods

Typically, assessments of environmental noise are based on a comparison of likely noise levels against either 'context' based limits or a set of fixed limits.

Context based limits are set relative to the existing noise environment and may also consider the characteristics of the noise source(s), whilst fixed limits are usually set regardless of the existing noise environment or type of noise source(s).

### 3.2.1 'Context' Based Limits (BS 4142:2014 +A1:2019)

BS 4142:2014+A1:2019 is commonly used to assess the potential impacts of new industrial sound sources on nearby receptors.

The BS 4142 form of assessment is based on the predicted or measured levels of an assessed sound source compared to the measured background sound levels without the specific sound source present and uses, "outdoor sound levels to assess the likely effects of sound on people who might be inside or outside a dwelling or premises used for residential purposes upon which sound is incident".

BS4142 uses the following definitions;

- Ambient Sound: Totally encompassing sound in a given situation at a given time, usually
  composed of sound from many sources, both near and far. Described using the metric, L<sub>Aeq</sub>
  (t).
- **Specific Sound Level**: Equivalent continuous A-weighted sound pressure level produced by the specific sound source at the assessment location over a given reference time interval, *Tr*. Described using the metric L<sub>Aeq (t)</sub>. Also referred to in this Appendix as the *Immission Level*.
- **Residual Sound Level**: Equivalent continuous A-weighted sound pressure level of the residual sound without the specific sound source(s) present at the assessment location over a given time interval, *T*. Described using the metric L<sub>Aeq (t)</sub>.
- **Background Sound Level**: A-weighted sound pressure level that is exceeded by the residual sound at the assessment location for 90% of a given time interval, *T*, measured using time weighting *F* and quoted to the nearest whole number of decibels. Described using the metric L<sub>A90 (t)</sub>.
- Rating Level: The Specific Sound Level adjusted for the characteristics of the sound. The
  Rating Level is calculated by adding a penalty or penalties (if required) to the Specific Sound
  Level when the sound source contains audible characteristics such as tonal, impulsive or
  intermittent components. Described using the metric, L<sub>Aeq (t)</sub>.

### 3.2.2 Fixed Guideline Levels (BS 8233:2014)

BS 8233 'Guidance on sound insulation and noise reduction for buildings' (1) presents guideline noise levels for daytime and night-time periods for a number of different building types; for residential areas these are based on guidelines issued by the World Health Organisation (WHO). Specifically, the





Standard states; "In general, for steady external noise sources, it is desirable that the internal ambient noise level does not exceed the guideline values in Table 4." Table 4 is reproduced here as Table 3-1.

Table 3-1: Indoor Ambient Noise Levels for Dwellings (BS 8233:2014 Table 4)

Activity	Location	07:00 to 23:00	23:00 to 07:00
Resting	Living room	35 dB L <sub>Aeq(16hour)</sub>	<u>.</u>
Dining	Dining room/area	40 dB L <sub>Aeq(16hour)</sub>	-
Sleeping (daytime resting)	Bedroom	35 dB L <sub>Aeq(16hour)</sub>	30 dB L <sub>Aeq(8hour)</sub>

A typical 13 dB attenuation value can be assumed for a partially opened window in accordance with the Acoustics, Ventilation and Overheating Guide (AVO) Appendix C (January 2020, published by the Association of Noise Consultant). This can be used as a reasonable value in order to convert between internal and external sound levels and limits. Therefore, an assessment of external noise levels can assume an external noise level limit of 13 dB above those values detailed within Table 3-1 (i.e. to achieve an internal night-time level of 30 dB  $L_{Aeq(8hour)}$  with windows open the external sound level must not exceed 43 dB  $L_{Aeq(8hour)}$ )

#### 3.3 Calculation Method

### 3.3.1 Noise Propagation Model (ISO 9613-2:2996)

To predict the noise immission levels attributable to the proposed BESS a noise propagation model was created using the propriety noise modelling software CadnaA. Within the software, complex models can be produced to simulate the propagation of noise according to a wide range of international calculation standards.

For this assessment noise propagation was calculated in accordance with ISO 9613 'Acoustics – Attenuation of Sound During Propagation Outdoors (2) using the following input parameters:

- Temperature is assumed to be 10 °C and relative humidity as 70%;
- A ground attenuation factor of 0.5 (semi-soft ground) has been used; and
- Receiver heights have been set to 4m.

#### 3.3.2 Uncertainties and Limitations

The noise propagation model is designed to give a good approximation of the specific sound level and the contribution of each individual sound source; however, it is expected that measured levels are unlikely to be matched exactly with modelled values and the following limitations in the model should be considered:

- In accordance with ISO 9613, all assessment locations are modelled as downwind of all sound sources and propagation calculations are based on a moderate ground-based temperature inversion, such as commonly occurs at night. These conditions are favourable to noise propagation;
- Table 5 of ISO 9613 estimates overall accuracy for broadband noise predictions of ± 3 dB, with average source to receiver heights <5m, at distances of up to 1,000m;



- The predicted barrier attenuation provided by local topography, embankments, walls, buildings and other structures in the intervening ground between source and receiver can only be approximated and not all barrier attenuation will have been accounted for; and,
- The model assumes all sound sources are operating continuously, simultaneously and at maximum noise output.

Modelled sound sources represent candidate plant only and an indicative site layout. The noise output of individual items of plant may vary from what is presented in this report after final plant specification and procurement.



# 4 Baseline Sound Level Monitoring ?

TNEI also undertook an operational wind turbine noise assessment for the Proposed Wind Farm. As part of the study, TNEI undertook background noise monitoring for an extended period between 26<sup>th</sup> January 2023 and 5<sup>th</sup> of April 2023 at seven neighbouring properties.

Table 4-1 details all seven Noise Monitoring Locations (NMLs), which are being used in this assessment. The NMLs are also shown in Figure A5.1 included within Annex 5.

**Table 4-1: Baseline Noise Monitoring Locations** 

NML	Approximate Distance and bearing to BESS Coordinat plant (m)		s (ITM X, Y)
NML01	1100 m north east	664333	670281
NML02	1000 m north east	664721	669755
NML03	1750 m south east	665105	668234
NML04	2200 m south	663548	667162
NML05	1670 m south west	662658	668128
NML06	1200 m west	662547	669183
NML07	1500 m north west	662653	670357

The noise monitoring equipment installed at the NMLs consisted of Rion NL-31's, Rion NL-32's and a Rion NL-52 Sound Level Meter (SLM), fitted with appropriate environmental wind shields. All noise monitoring equipment (calibrator, SLM and microphones) used for the study are categorised as Class 1, as specified in IEC 61672-1 'Electroacoustics. Sound level meters. Specifications' (3). The equipment was calibrated onsite at the beginning and end of each measurement period with no significant deviations noted.

Wind speed and direction data was measured continuously during the noise survey using a LIDAR unit, which was temporarily installed within the Proposed Project site. For operational wind farm noise assessments, the measured noise data is organised into wind speed 'bins' in order to determine wind-speed specific noise limits. In contrast, BS 4142 states, "Exercise caution when making measurements in poor weather conditions, such as wind speeds greater than 5 m/s." Accordingly, the noise data was filtered to remove any data points that were measured during periods of high wind speeds and rain. In this particular case, all noise data measured with wind speeds at or above 5ms<sup>-1</sup> has been removed. It should be noted that the wind speed data used in this assessment is based on measurements made at wind speeds at 10m height (standardised).



Table 4-2 details the representative background sound levels, L<sub>A90 (10mins)</sub>, which have been determined after considering the distribution of data for each measurement period. Typically, baseline sound level measurements made in accordance with BS 4142 are undertaken in 15-minute periods. However, as the baseline data was measured as part of the operational wind turbine noise assessment, a 10-minute measurement period was adopted for use as part of this assessment. Annex 3 contains the statistical and distribution analysis charts used to ascertain the representative background sound levels.

Table 4-2: Representative Background Sound level, dB LA90(10mins)

NML ID	Daytime L <sub>A90(10mins)</sub>	Night-time L <sub>A90(10mins)</sub>
NML01	25	20
NML02	27	22
NML03	32	25
NML04	36	21
NML05	33	23
NML06	29	22
NML07	32	22



# 5 Operational Noise Impacts

### 5.1 Modelling of Individual Sound Sources

The noise model considers all of the sound sources detailed within Section 2.1 and the following paragraphs describe how each sound source has been incorporated into the noise model.

Noise modelling is based on candidate plant typical for the size and class of the Proposed Project and, where possible, data sheets for candidate items of plant have been provided within Annex 4. It should be noted that final plant specifications will vary during detailed design and the tendering process.

The sound sources considered within this assessment are assumed as follows:

- 64 x Fluence Cubes;
- 2 x Chint Electric MV Transformer;
- 4 x PE HEMK PCSK Inverter; and
- 1 x HV Grid Transformer

These plant items have been located in a noise model according to the layout included in Annex 2.

#### 5.1.1 Fluence Cube and MV Transformer

TNEI have used noise data for a Fluence Cube, offered by the supplier, Fluence.

Each Fluence Cube includes a number of internally and externally located sound sources, most notably the HVAC and chiller units, which are housed within the Cube.

Chint Electric MV Transformers and Power Electronics (PE) E HEMK PCSK Inverter were also assumed.

The noise data for the Cubes, MV Transformers and Inverters has been provided to TNEI under a Non-Disclosure Agreement and as such detailed noise level data cannot be provided in this report. TNEI would be happy to discuss this data in more detail with the Planning Authority, if required.

### 5.1.2 High Voltage (HV) Grid Transformer

A HV Grid Transformer near the proposed BESS compound has been assumed. The model assumed within the noise model is a ONAF (Oil Natural, Air Forced) Ganz HV transformer with a broadband sound pressure level (SPL) value of 68 dBA at 2m, which is approximately equivalent 82 dBA SWL.

No spectral data is available for this candidate, however, typical HV transformer spectra is well documented and 1/3 Octave Band SWL data for a similar unit has been input into the noise model and transposed to equal a broadband SWL of 82 dBA. Table 5-1 details the resulting SWL used within the noise model and the relevant data sheets are included within Annex 4.

Table 5-1: 1/3 Octave Band SWL, dBA used to model the HV Grid Transformer

		Frequency (Hz)							
Hz	25	31.5	40	50	63	80	100	125	160
dBA	-	-	-	58	42	49	66	62	72
Hz	200	250	315	400	500	630	800	1000	1250



	Frequency (Hz)								
dBA	68	70	74	71	71	73	72	771	68
Hz	1600	2000	2500	3150	4000	5000	6300	8000	10000
dBA	66	64	62	61	61	59	56	54	520

### 5.2 Noise Character

### 5.2.1 Tonality

Power transformers are inherently tonal at source in the 100 Hz frequency band, therefore it is important to consider whether a 100Hz tone might be audible at the receptors. Based on TNEIs experience of similar developments and given the relatively large distance between source and receiver, we do not expect a tone to be perceptible at either BESS Noise Assessment Location (BNAL). As such, no tonal penalty has been applied.

### 5.2.2 Impulsivity

Impulsivity is not considered to be a relevant sound characteristic of a transformer or BESS when operational, as the noise level will be predictable and consistent.

### 5.2.3 Intermittency

As with impulsivity, intermittency is not considered to be a relevant sound characteristic in this case. Once operational, the proposed BESS compound and associated plant will be operational for extended durations and will only likely shut down for maintenance purposes. Therefore, the noise is predictable and consistent and not considered to be intermittent.

#### 5.2.4 Overall Character Correction

With due regard to the above, no character corrections are required.

### 5.3 Calculated Immission Levels

Noise immission levels have been calculated at 18 BESS Noise Assessment Locations (termed BNALs), which have been selected to represent the closest NSRs. The BNALs have been set on the side of the property facing the proposed BESS compound, representing the closest point of the property's amenity area. The BNALs are detailed in Table 5-2 and shown on Figure A5.1 within Annex 5.

Table 5-2: BESS Noise Assessment Locations (BNALs)

BNAL ID	ITM X	ITM Y
BNAL01	662730	670033
BNAL02	662612	670155
BNAL03	663257	670292
BNAL04	663822	670342



BNAL ID	ITM X	<b>₹</b> ITM Y
BNAL05	664335	670302
BNAL06	664472	670214
BNAL07	664688	669900
BNAL08	664705	669725
BNAL09	664928	669208
BNAL10	664824	668894
BNAL11	664698	668149
BNAL12	664248	667759
BNAL13	663159	667611
BNAL14	662682	668090
BNAL15	662840	669042
BNAL16	662569	669160
BNAL17	661841	668376
BNAL18	662639	667483

The immission levels are calculated assuming all plant is operating continuously and concurrently. The levels are detailed in Table 5-3 as dB  $L_{Aeq(t)}$ . No time period is specified as the model assumes that noise levels will not fluctuate and will remain the same for all time periods.

Table 5-3: Predicted Immission Levels, dB  $L_{\text{Aeq(t)}}$ 

Noise Assessment Location, BNAL ID	Immission Level, dB L <sub>Aeq(t)</sub>
BNAL01	26
BNAL02	25
BNAL03	29
BNAL04	29
BNAL05	28
BNAL06	28



Noise Assessment Location, BNAL ID	Immission Level, 48 L <sub>Aeq(t)</sub>
BNAL07	27 E
BNAL08	26 24 20 20 20 20 20 20 20 20 20 20 20 20 20
BNAL09	24
BNAL10	27
BNAL11	23
BNAL12	23
BNAL13	25
BNAL14	24
BNAL15	29
BNAL16	26
BNAL17	19
BNAL18	24



#### Noise Impact Assessment 6

#### 6.1 Noise Limit Criteria

PECENED. A fixed noise level limit assessment has been adopted rather than undertaking an assessment against background sound levels. This is because at the NMLs, particularly during the night-time, background sound levels are very low (20 dB LA<sub>90(10mins)</sub> in some cases) and as such it may not be appropriate to rely on BS 4142 as the appropriate assessment method. In this regard the ANC BS 4142 Technical Note states<sup>1</sup>;

"The standard states that the absolute level of sound can be of significance, where the residual values are low and where they are high and should be taken into account when determining the overall impact of a particular specific sound source. The second paragraph notes that absolute levels may be as, or more, important than relative outcomes where background and rating levels are low. It is important to note that both background and rating levels would need to be low for this particular caveat to apply.

BS 4142 does not indicate how the initial estimate of impact should be adjusted when background and rating levels are low, only that the absolute levels may be more important than the difference between the two values. It is likely that where the background and rating levels are low, the absolute levels might suggest a more acceptable outcome than would otherwise be suggested by the difference between the values. For example, a situation might be considered acceptable where a rating level of 30 dB is 10 dB above a background sound level of 20 dB, i.e., an initial estimate of a significant adverse impact is modified by the low rating and background sound levels.

There may be situations where the opposite is true, and it is for the assessor to justify any modifications to the initial estimate of impact. BS 4142 does not define 'low' in the context of background sound levels nor rating levels. The note to the Scope of the 1997 version of BS 4142 defined very low background sound levels as being less than about 30 dB  $L_{A90}$ , and low rating levels as being less than about 35 dB L<sub>Ar.Tr</sub>. The WG [Working Group] suggest that similar values would not be unreasonable in the context of BS 4142, but that the assessor should make a judgement and justify it where appropriate."

In this case, as defined in BS4142:1997 and acknowledged in the ANC Technical Note:

- The measured background sound levels are 'very low' i.e. below 30 dB L<sub>A90</sub>; and,
- The Rating Level is low i.e. below 35 dB L<sub>Ar,Tr</sub>

Accordingly, it is felt that the use of fixed noise level limits, as opposed to context based limits is the most appropriate form of assessment and this assessment approach has previously been used by TNEI and agreed with some Local Authorities in the UK for similar projects where measured background sound levels in rural areas were similarly low.

#### 6.2 **Quantitative Assessment**

An assessment is detailed below against the most stringent of the guideline levels presented in BS 8233:2014. To determine a set of external limits, 13 dB has been added to the BS 8233 internal levels to allow for the attenuation provided by a partially open window, as detailed in Table 6-1.

<sup>&</sup>lt;sup>1</sup> Underlining added by TNEI for emphasis.





Table 6-1: Derived BS 8233 Fixed Level Limits

Table 6-1: Derived 65 8253	Fixed Level Limits	<b>P</b>			
Assessment Parameter	BS 8233 Guideline Level (dB LAeq,t)	Allowance for Open Window Attenuation (dB LAeq,t)	Equivalent/External Level		
Daytime 07:00-23:00	35	13	48		
Night-time 23:00-07:00	30	13	43		

Table 6-2 below compares the predicted immission levels at the BNALs with the derived noise limits.

**Table 6-2: Quantitative Assessment** 

	Daytime		Night-time	
Noise Assessment Location, BNAL ID	Immission Level, dB L <sub>Aeq(t)</sub>	Margin above/below Noise Level Limit, dB	Immission Level, dB L <sub>Aeq(t)</sub>	Margin above/below Noise Level Limit, dB
BNAL01	26	-22	26	-17
BNAL02	25	-23	25	-18
BNAL03	29	-19	29	-14
BNAL04	29	-19	29	-14
BNAL05	28	-20	28	-15
BNAL06	28	-20	28	-15
BNAL07	27	-21	27	-16
BNAL08	26	-22	26	-17
BNAL09	24	-24	24	-19
BNAL10	27	-21	27	-16
BNAL11	23	-25	23	-20
BNAL12	23	-25	23	-20
BNAL13	25	-23	25	-18
BNAL14	24	-25	24	-20
BNAL15	29	-19	29	-14
BNAL16	26	-22	26	-17



	Daytime		Night-time	
Noise Assessment Location, BNAL ID	Immission Level, dB L <sub>Aeq(t)</sub>	Margin above/below Noise Level Limit, dB	Immission Level, dB L <sub>Aeq(t)</sub>	Margin Dove/below Note Level Limit dB
BNAL17	19	-29	19	-24
BNAL18	24	-24	24	-19

As can be seen, the predictions are at least 13dB below the threshold levels of BS 8233 and no significant noise impact is predicted. No noise mitigation measures are required for the proposed BESS compound.



## 7 Summary

In order to assess the impact of noise emissions from the proposed BESS compound within the Proposed Project, TNEI has produced a noise propagation model in accordance with ISO 9613 that predicts the noise immission levels at the nearest identified residential receptors, based on abyout and candidate plant that is typical for this type of BESS development. A small number of residential properties was identified and assessed, the nearest of which is approximately 950 m to the proposed BESS compound.

A baseline survey was undertaken as part of the Proposed Wind Farm operational noise assessment to determine background sound levels in the vicinity. The resulting low levels of measured background sound, alongside with low predicted Rating Levels, indicates that the methodology of BS 4142 is not appropriate. As such, fixed guideline levels detailed in BS 8233 were used for both daytime and night-time assessment periods.

The assessment results shows that noise predictions are at least 13dB below the threshold levels of BS 8233 and no significant noise impact is predicted. No noise mitigation measures are required for the proposed BESS.



### 8 References

- 1. **British Standards Institute.** *Guidance on Sound Insulation and Noise Reduction for Buildings.* UK : BSI, 2014. BS8233:2014.
- 2. **(ISO), International Organization for Standardization.** *Acoustics Attenuation of Sound During Propagation Outdoors: Part 2 General Method of Calculation.* Geneva : (ISO), International Organization for Standardization, 1996. ISO 9613-2:1996.
- 3. **Commission Electrotechnique Internationale (IEC).** *Electroacoustics Sound level meters Part 1: Specifications.* Geneva: IEC, 2013. IEC 61672-1:2013.
- 4. **British Standards Institute.** *Methods for Rating and Assessing Industrial and Commercial Sound.* UK: BSI, 2014. BS4142:2014 + A1:2019.
- 5. **Association of Noise Consultants.** *ANC Good Practice Working Group, BS 4142:2014+A1:2019 Technical Note. s.1.* 2020.



# Annex 1 – Glossary of Terms

**Attenuation:** the reduction in level of a sound between the source and a receiver due to any combination of effects including: distance, atmospheric absorption, acoustic screening, the presence of a building façade, etc.

**Background Sound Level:** the sound level rarely fallen below in any given location over any given time period, often classed according to daytime, evening or night-time periods. The LA90 indices (see below) are typically used to represent the background sound level.

Broadband Noise: noise with components over a wide range of frequencies.

**Decibel (dB):** the ratio between the quietest audible sound and the loudest tolerable sound is a million to one in terms of the change in sound pressure. A logarithmic scale is used in sound level measurements because of this wide range. The scale used is the decibel (dB) scale which extends from 0 to 140 decibels (dB) corresponding to the intensity of the sound level.

**dB(A):** the ear has the ability to recognise a particular sound depending on its pitch or frequency. Microphones cannot differentiate sound in the same way as the ear, and to counter this weakness the sound measuring instrument applies a correction to correspond more closely to the frequency response of the human ear. The correction factor is called 'A Weighting' and the resulting measurements are written as dB(A). The dB(A) weighting is internationally accepted and has been found to correspond well with people's subjective reaction to sound levels and noise. Some typical subjective changes in sound levels are:

- a change of 3 dB(A) is just perceptible;
- a change of 5 dB(A) is clearly perceptible; and
- a change of 10 dB(A) is twice (or half) as loud.

**Directivity:** the property of a sound source that causes more sound to be radiated in one direction than another.

**Emission:** the sound energy emitted by a sound source (e.g. a wind turbine).

**Frequency:** the pitch of a sound in Hz or kHz. See Hertz.

**Ground Effects:** the modification of sound at a receiver location due to the interaction of the sound waves with the ground along its propagation path from source to receiver. Described using the term 'G', and ranges between 0 (hard ground), 0.5 (mixed ground) and 1 (soft ground).

**Hertz (Hz):** sound frequency refers to how quickly the air vibrates, or how close the sound waves are to each other (in cycles per second, or Hertz (Hz)).

**Immission:** the sound pressure level detected at a given location (e.g. the nearest dwelling).

**Isopleth:** a line on a map connecting points of equal value, for example air pressure, noise level etc.

**Noise:** unwanted sound.



 $L_w$ : is the sound power level. It is a measure of the total sound energy radiated by a sound source and is used to calculate sound levels at a distant location. The  $L_{WA}$  is the A - weighted sound power level.

L<sub>eq</sub>: is the equivalent continuous sound level, and is the sound level of a steady sound with the same energy as a fluctuating sound over the same period. It is possible to consider this level as the ambient noise encompassing all noise at a given time. The L<sub>Aeq, T</sub> is the A - weighted equivalent continuous sound level over a given time period (T).

 $L_{90}$ : index represents the sound level exceeded for 90 percent of the measurement period and is used to indicate quieter times during the measurement period. It is often used to measure the background sound level. The  $L_{A90,10min}$  is the A - weighted background sound level over a ten-minute measurement sample.

Sound Level Meter: an instrument for measuring sound pressure level.

**Sound Pressure Level:** a measure of the sound pressure at a point, in decibels.

**Tonal Noise:** noise which covers a very restricted range of frequencies (e.g. a range of ≤20 Hz). This noise is subjectively more annoying than broadband noise.

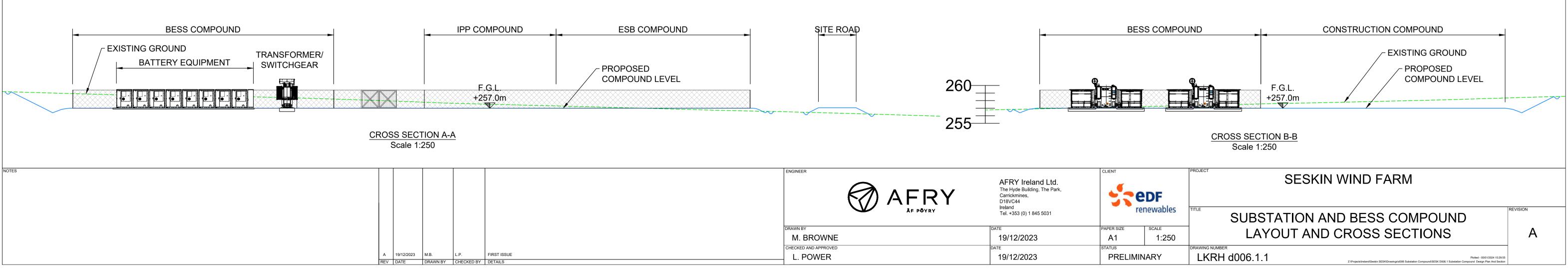


# Annex 2 – Development Information

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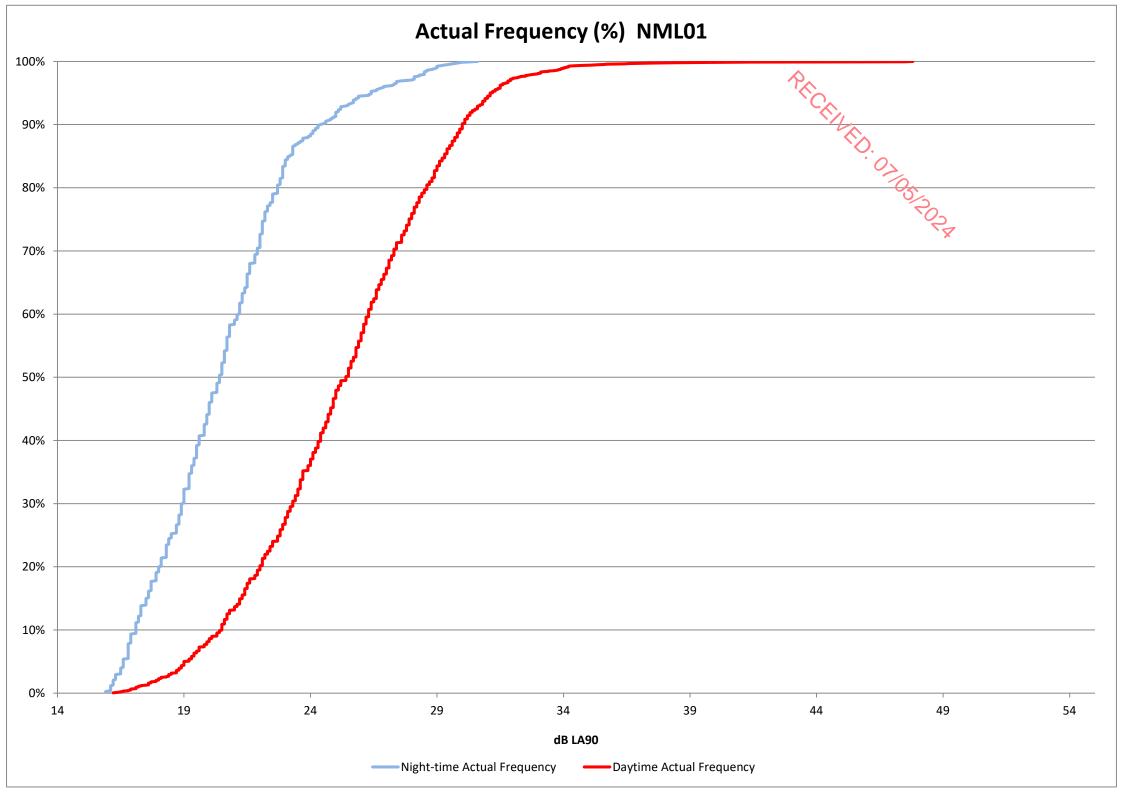


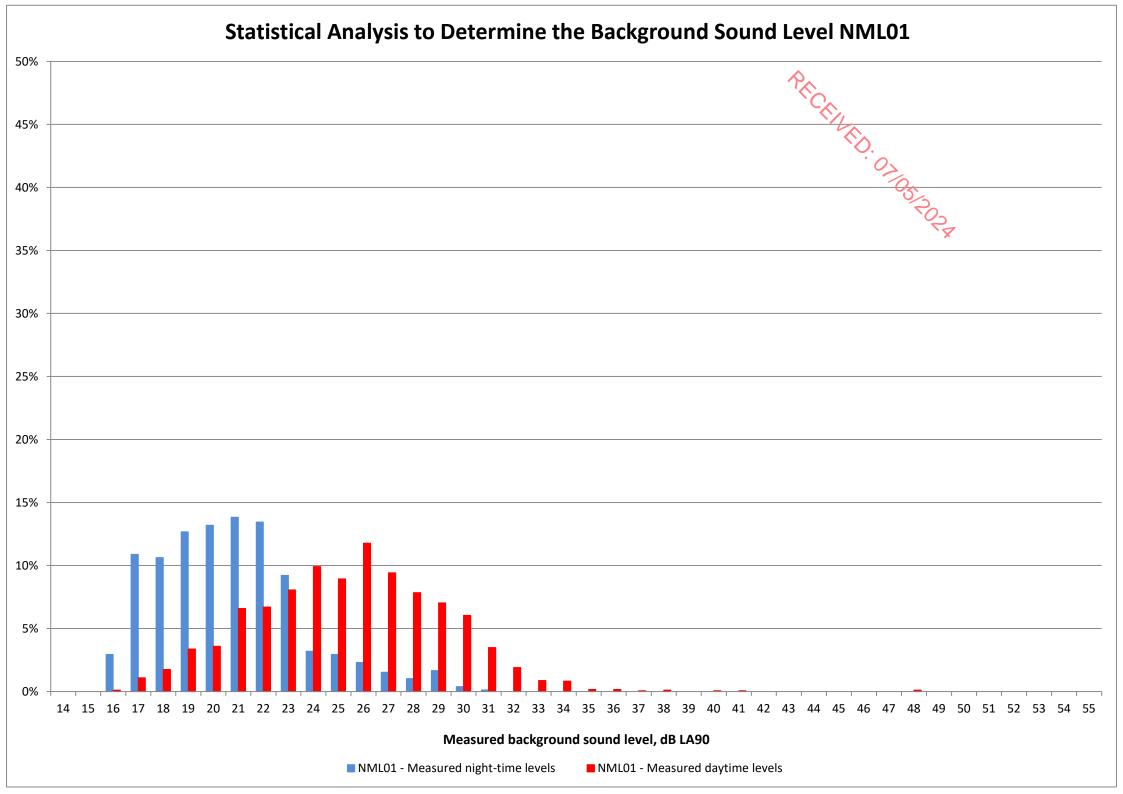


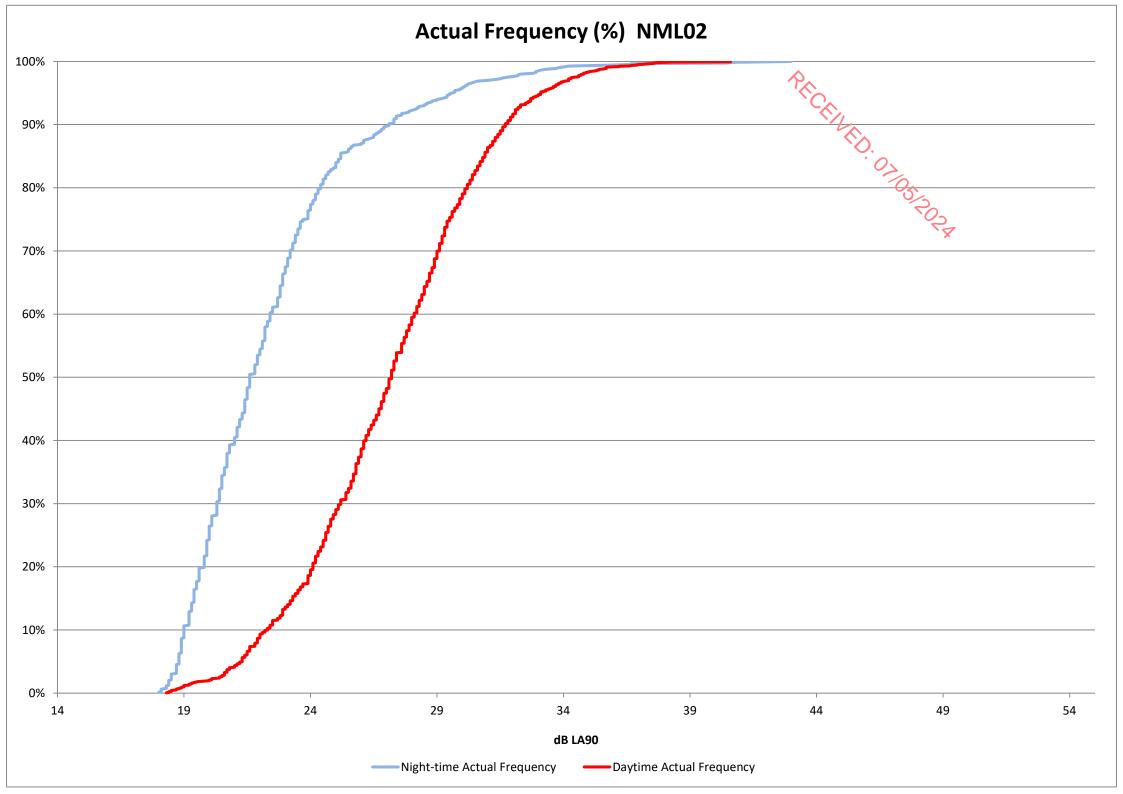
# Annex 3 - Baseline Survey Data

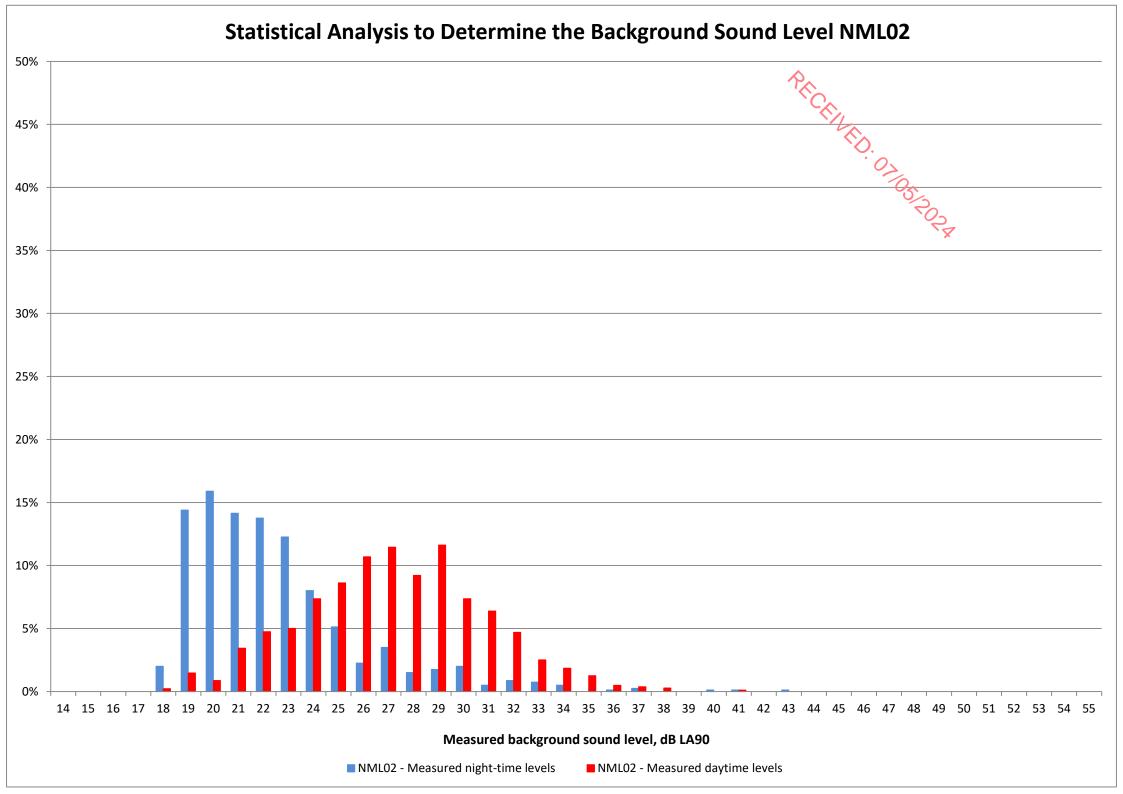
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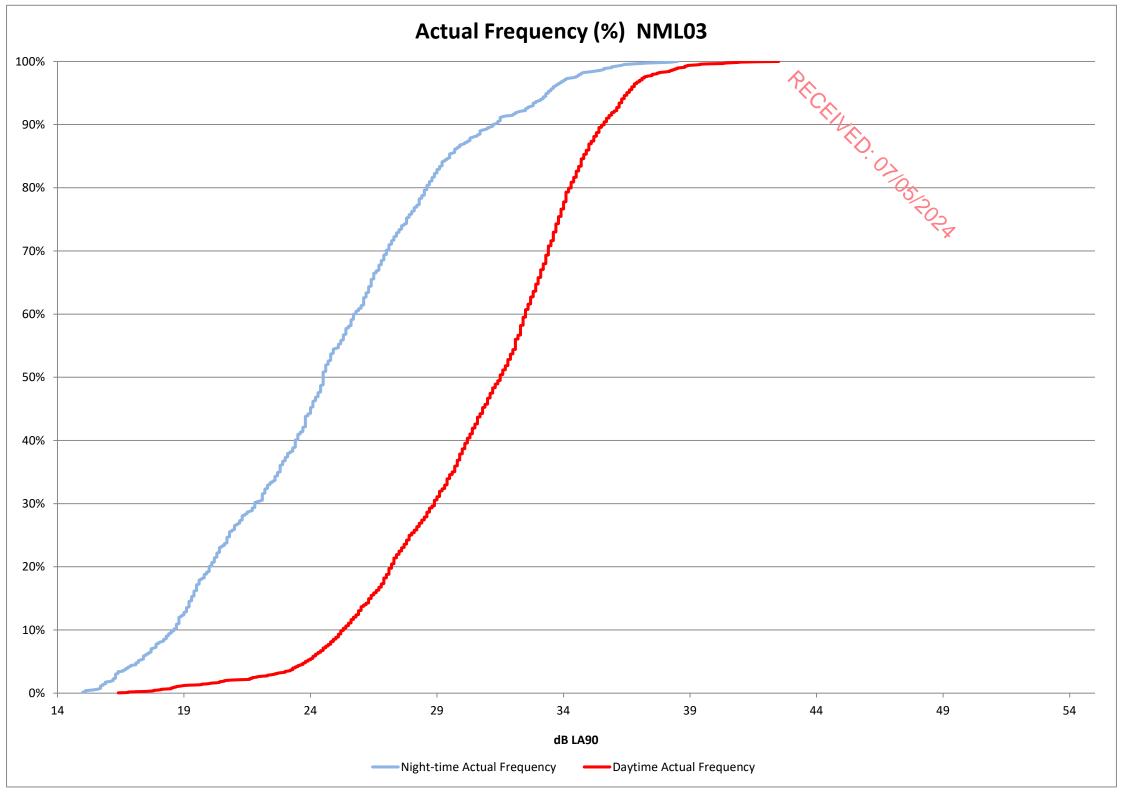


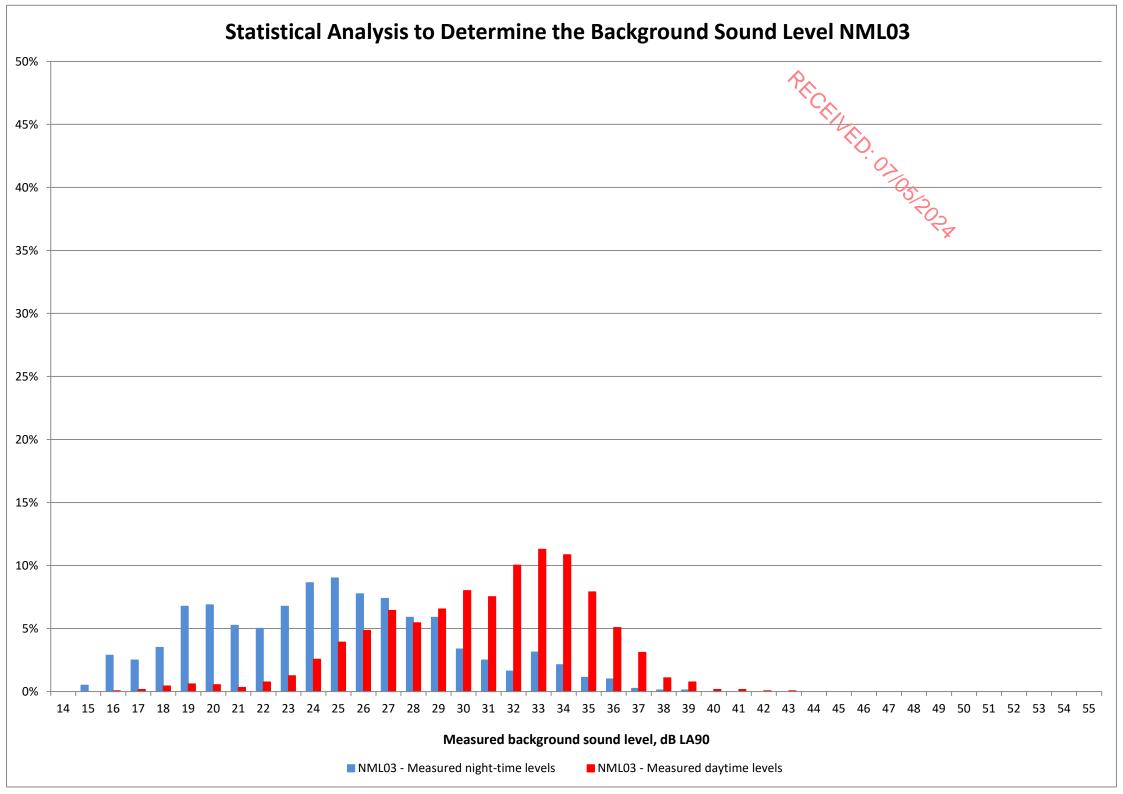


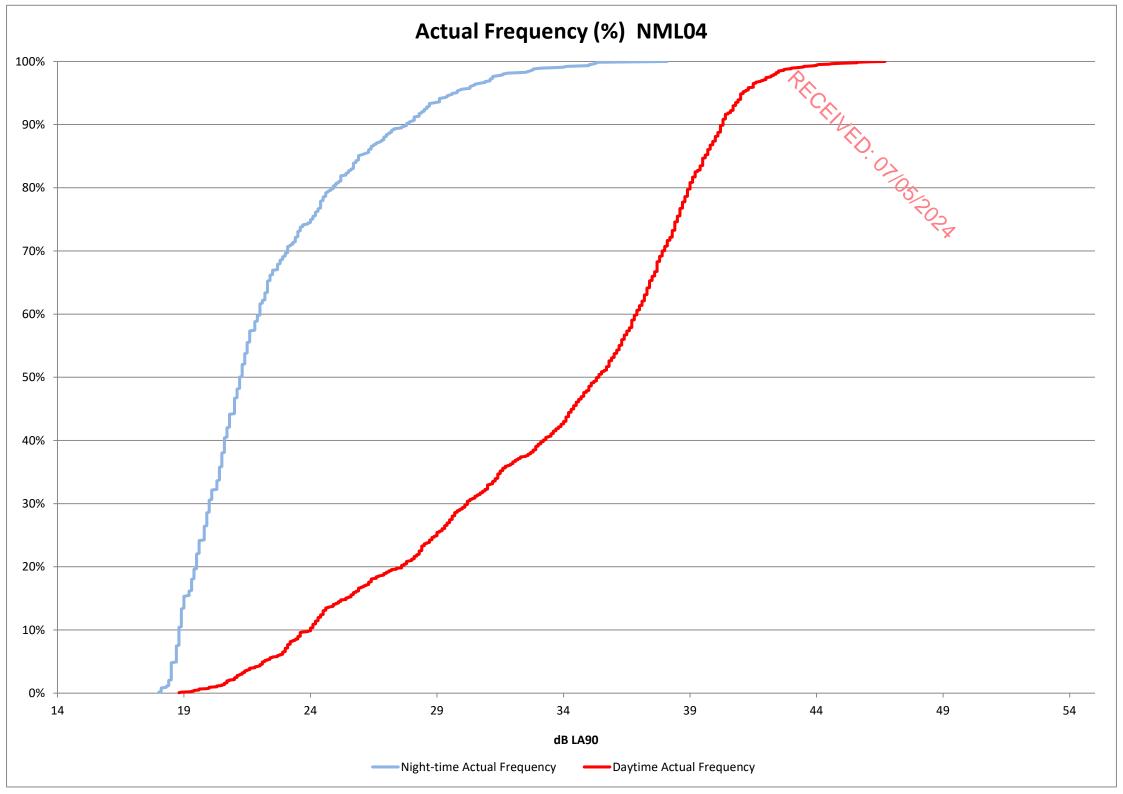


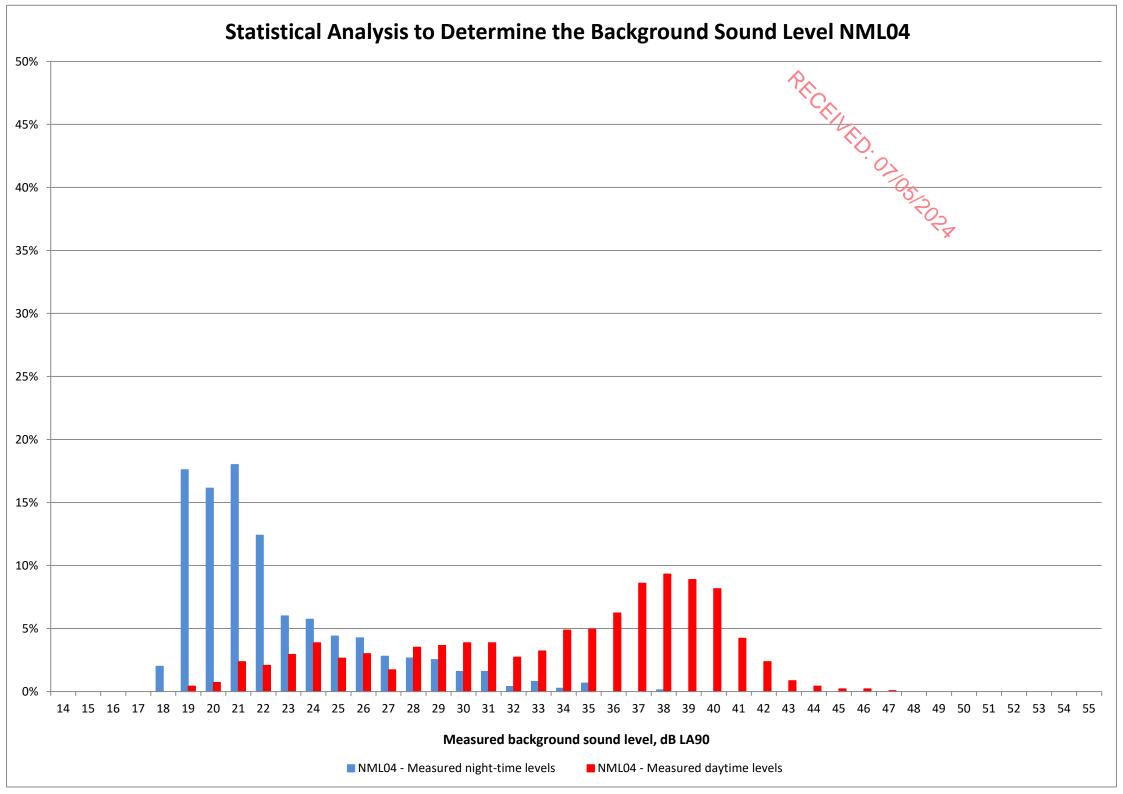


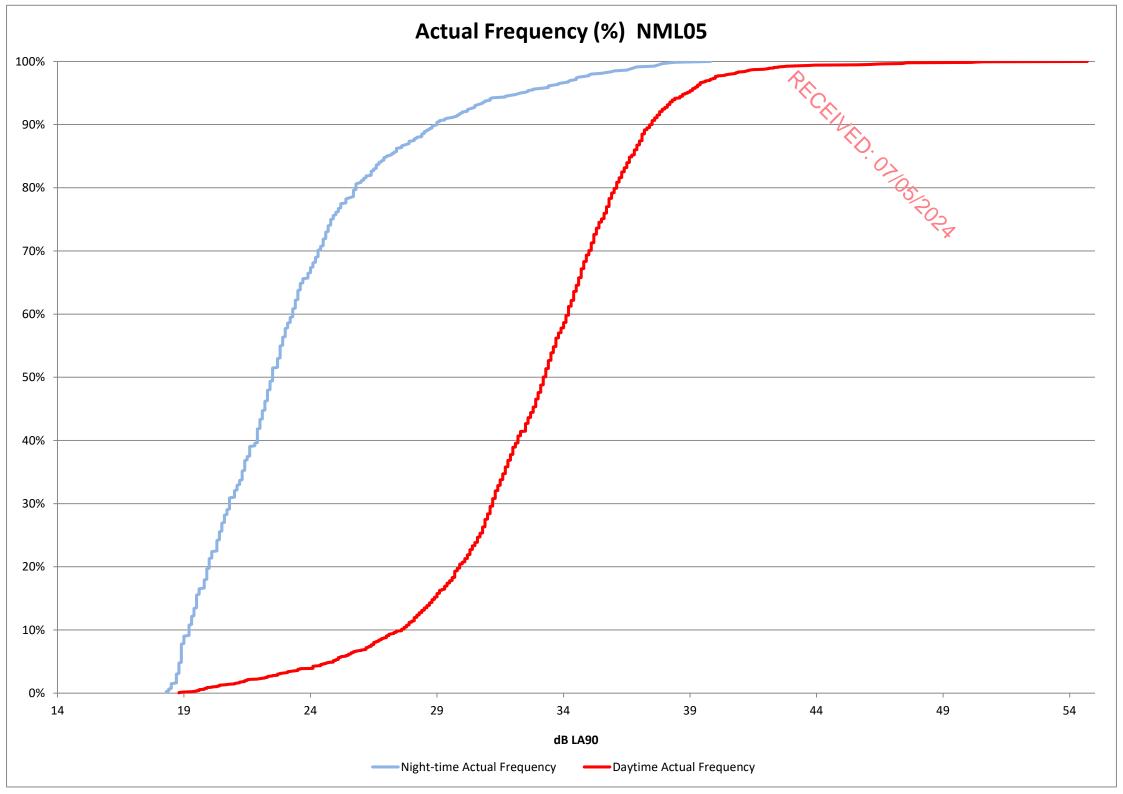


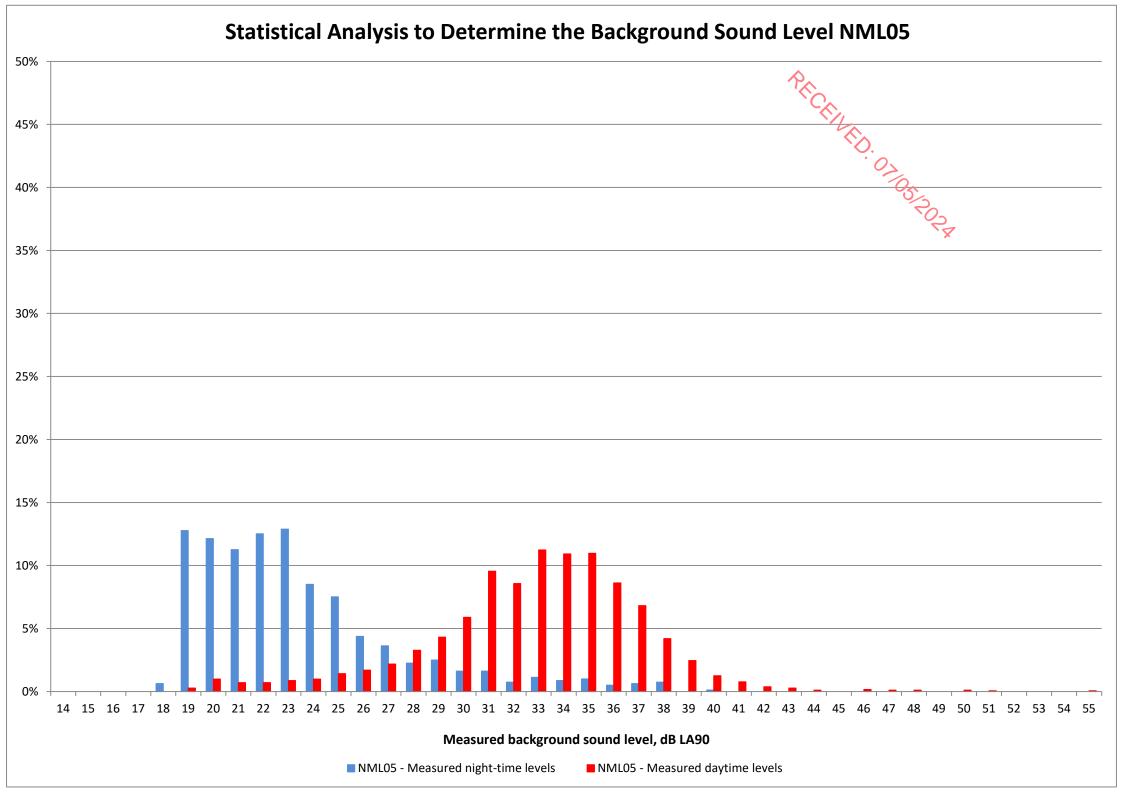


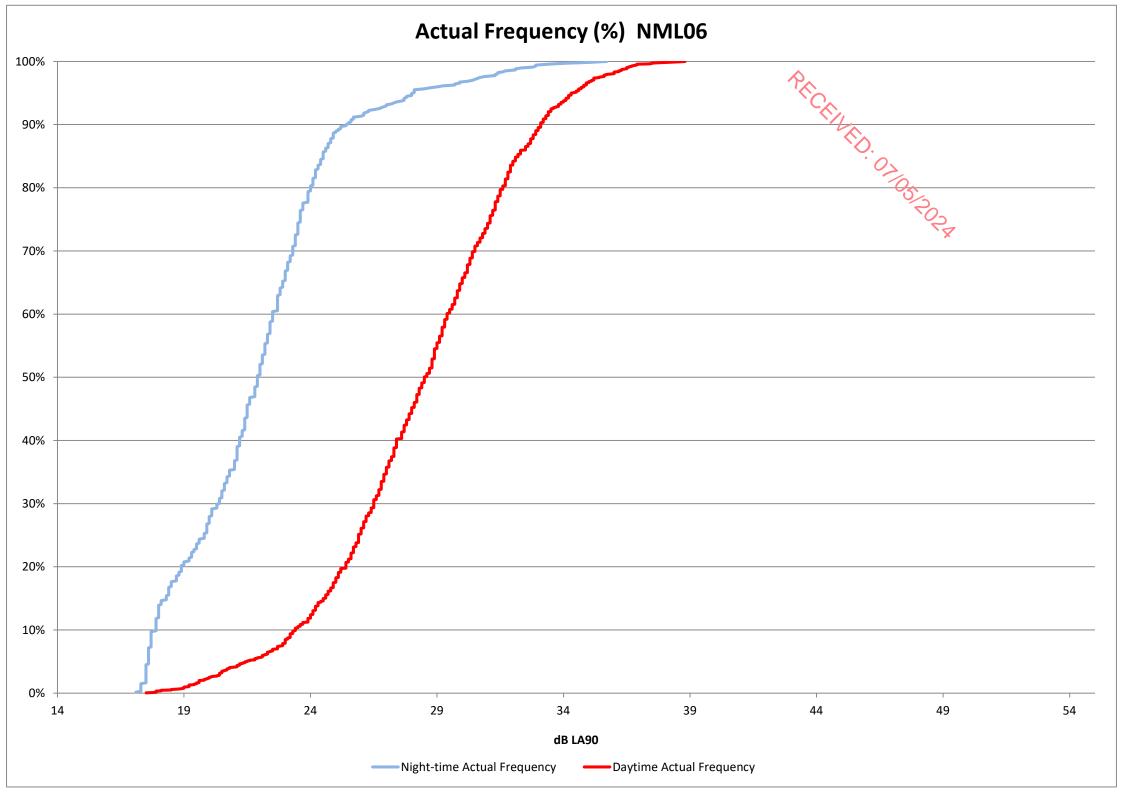


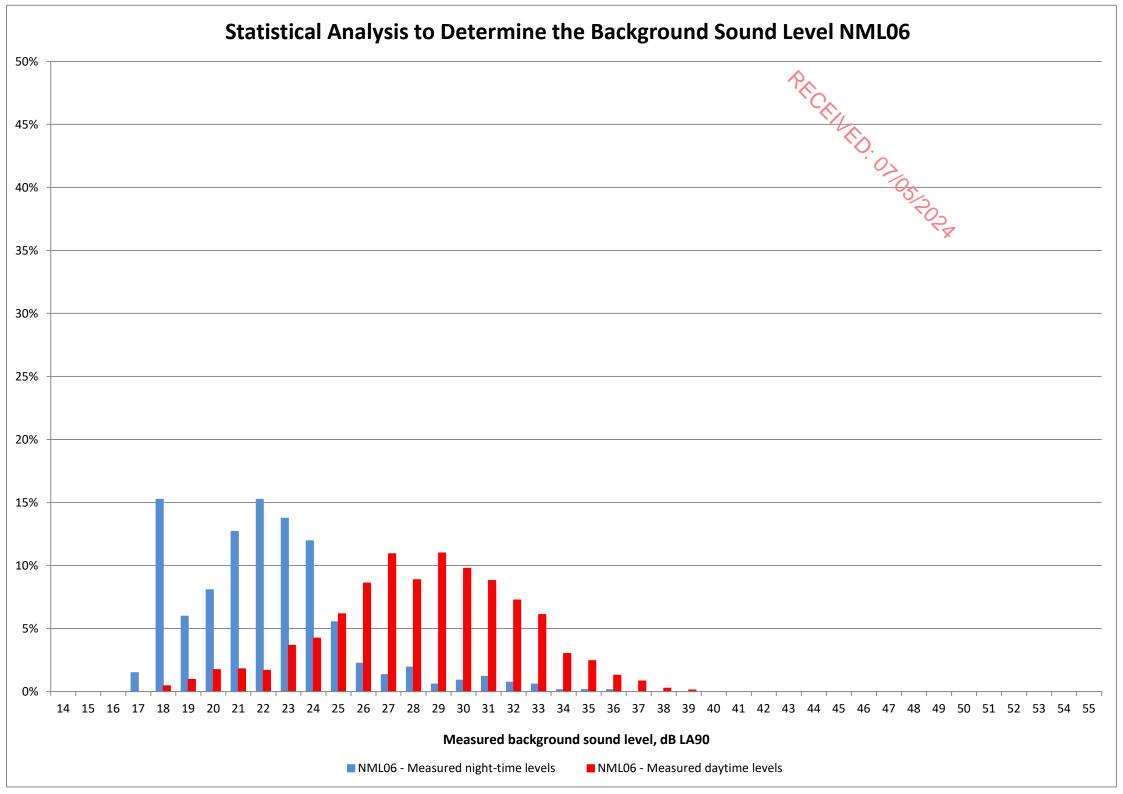


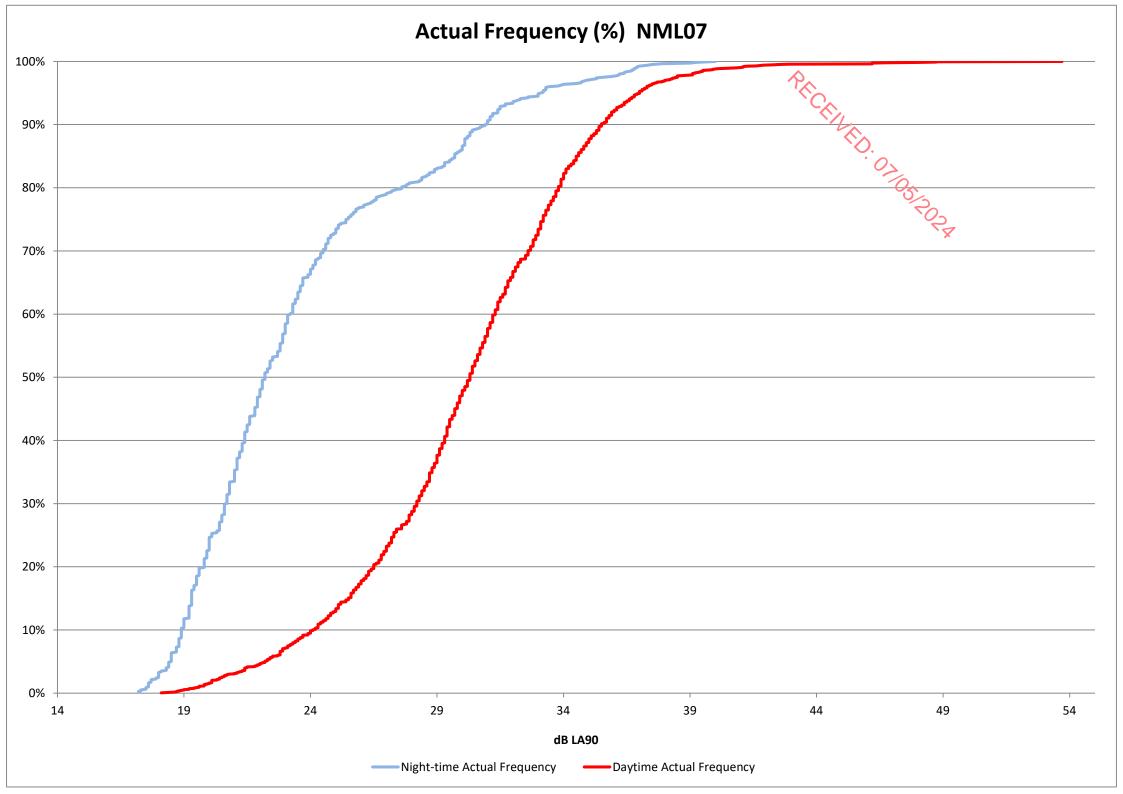


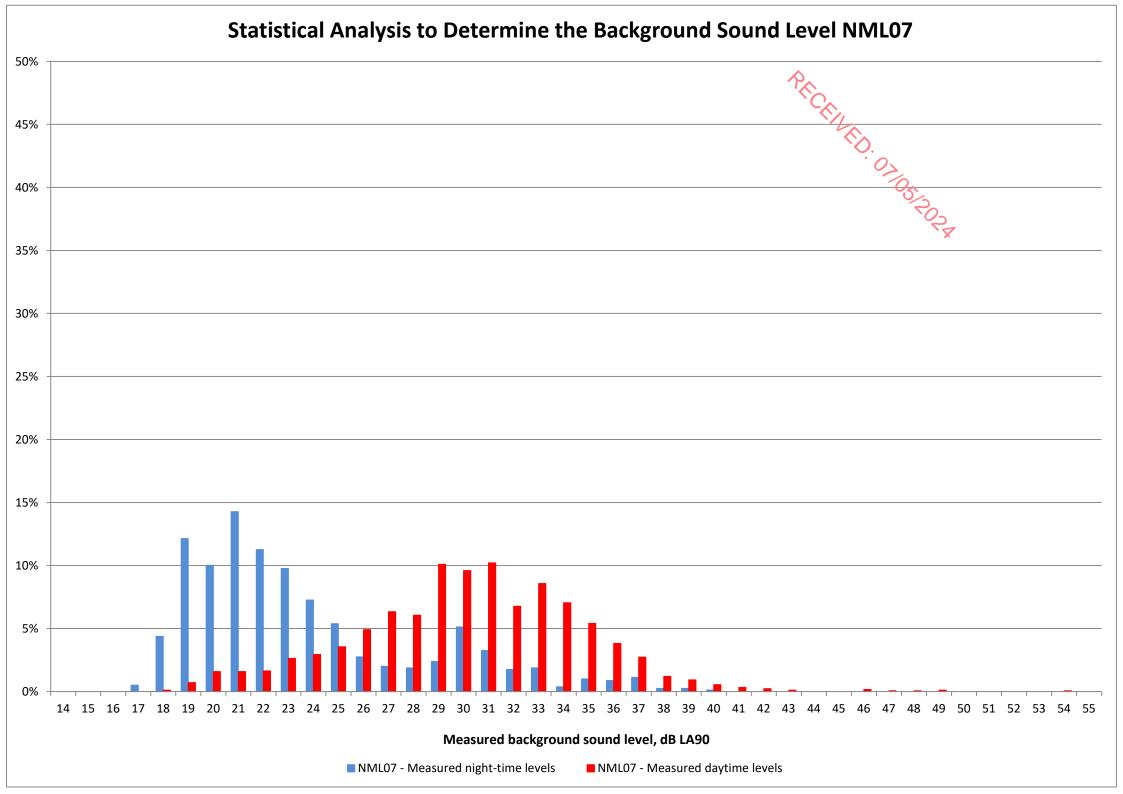












# Annex 4 – Noise Modelling Data

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20.	Guaranteed noise level acc. to IEC 60076-10					100	
	Sound pressure level at 100%Un, 100%In at	ONAN	65	dB(A)	at	0.3 m	)
	10017	ONAF	68	dB(A)	at	2.0 n	
21.	Dimensions and masses (approx.)						· O.
	Length		9,000	mm			70
	Width		5,600	mm			(M)
	Height		6,400	mm			· 07/05/2024
	Oil mass		34,100	kg			×
	Total mass		167,800	kg			
	Transport dimensions and mass of heaviest pa	art (approx.)					
	Length		7,500	mm			
	Width		2,300	mm			
	Height		4,200	mm			
	Transport mass		112,300	kg	dry a	air filled	
	Estimated packing details per unit : see attach	ed Masses and	dimension s	heet			



### **TEST REPORT**

Serial No.: IZPL001134582

### Sound Level

### Combination of sound level measurements

Rated voltage	Applied voltage	Rated current	A pp led current	Tap position	Fans in operation	Pumps in operation
[96]	IkV1	[66]	[A]			
100	33	100	262.43		. 8	

(seathar,	deasurement!	dessurenent d	Combined
	Sound Power Level	sund Power Level	Sound Power Level
IRv1	IdB(A)1	IdB(A))	(dB(A)

Total Sound Level		76.9	87.8	88.2
	63	39.6	64.4	64.4
	125	59.5	79.6	79.6
	250	76.1	81.2	82.3
04	500	67.3	82.6	82.7
Octave Band	1000	56.3	81.7	81.7
	2000	51.6	75.4	75.4
	4000	54.1	71.3	71.4
	8000	57.4	64.2	65.0

	50	36.1	63.8	63.8
	63	37.0	47.4	47.8
	80	0.0	55.1	55.1
	100	58.4	71.9	72.1
	125	47.5	68.5	68.6
	160	51.3	78.4	78.4
	200	63.1	73.7	74.1
	250	60.9	76.4	76.5
	315	75.8	78.0	80.1
	400	61.2	77.0	77.1
	500	63.7	76.9	77.1
L. Outon Band	630	62.5	79.2	79.3
% Octave Band	800	53.7	78.6	78.6
	1000	51.4	76.7	76.7
	1250	47.1	74.5	74.5
	1600	47.0	72.4	72.4
	2000	45.7	70.2	70.2
	2500	45.9	68.5	68,5
	3150	48.4	67.5	67.6
	4000	49.6	66.9	67.0
	5000	49.9	64.8	64.9
	6300	51.2	61.5	61.9
	8000	52.9	58.8	59.8
	10000	53.6	56.4	58.2

Rated voltage	Applied voltage	Rated current	Applied current	Tap position	Fans in operation	Pumps in operation
[96]	DAV1	[99]	IAI	100000		

Frequency	Combined Sound Power Level
[Hz]	[dB(A)]

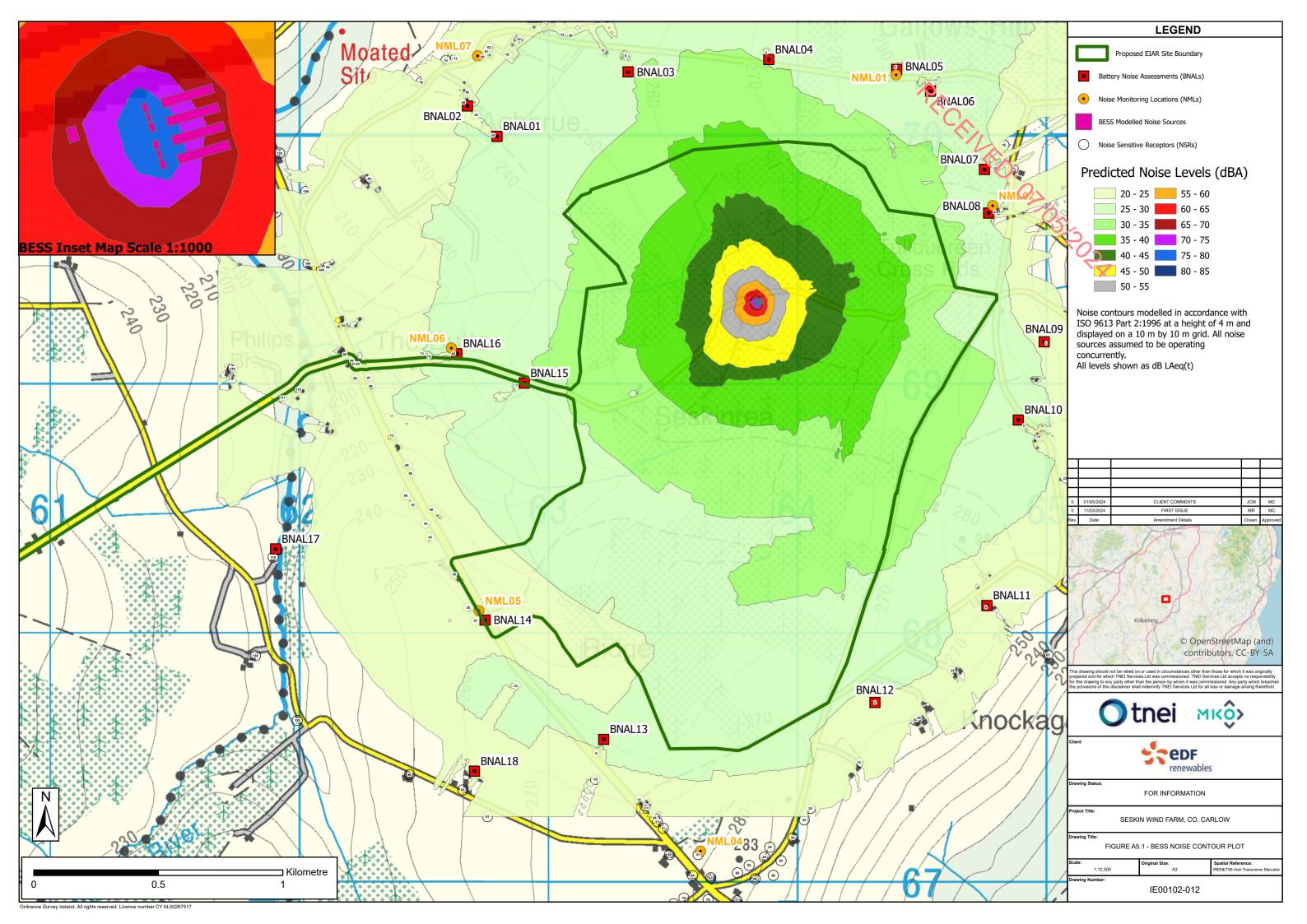
Total Sound Level					
	63				
	125				
	250				
0-1	500				
Octave Band	1000				
	2000				
	4000				
	8000				

	24		 
	63		
	80		
	100		
	125		
	160		
	200		
	250		 
	315		
	400		
	500		
% Octave Band	630		
25 Octave Dana	800		
	1000		
	1250		
	1600		
	2000		
	2500		
	3150		
	4000		
	5000		
	6300		
	8000		
The state of the s	10000		

## Annex 5 – Figures

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# Battery Energy Storage System (BESS) Noise Report Seskin Wind Farm, Co. Carlow Annex 6 — Quantitative assessments at ANSRs This corresponds to the corresponding to the corresp



### **BESS Quantitative Assessment at all NSRs**

		Day	time	Night	t-time	
	Immission Level,	Equivalent	Margin	Fautivalant	Margin	
H / BNAL	dB L <sub>Aeq(t)</sub>	External Level	above/below	Equivalent External Level	above/below	
	Aeq(t)	(dB LAeq,t)	Noise Level Limit, dB	(dB LAeq,t)	Noise Level Limit, dB	CENED. OF OS ROPA
H6(BNAL08)	26	48	-22	43	-17	.0
H7(BNAL09)	24	48	42	43	-19	
H8(BNAL12)	23	48	42	43	-20	5
H9(BNAL10)	27	48	43	43	-16	2
H10(BNAL05)	28	48	45	43	-15	2
H11(BNAL04)	29	48	44	43	-14	· ×
H12(BNAL03) H13(BNAL15)	27 28	48 48	42 47	43		4
H14(BNAL11)	23	48	47	43 43	-15 -20	†
H15(BNAL13)	25	48	45	43	-18	t
H16(BNAL07)	26	48	42	43	-17	†
H17(BNAL06)	27	48	44	43	-16	İ
H18	26	48	43	43	-17	
H19	27	48	41	43	-16	
H20	21	48	40	43	-22	
H21	24	48	44	43	-19	
H22	23	48	41	43	-20	4
H23	21	48	39	43	-22	ł
H24 H25(BNAL01)	24 26	48 48	44 43	43 43	-19 -17	†
H26	24	48	44	43	-19	t
H27	24	48	45	43	-19	İ
H29	23	48	41	43	-20	İ
H30	26	48	46	43	-17	
H31	22	48	41	43	-21	
H32	22	48	40	43	-21	ļ
H33	24	48	45	43	-19	
H34	24	48	45	43	-19	ł
H35 H36	21 21	48 48	40 40	43 43	-22 -22	ł
H37	25	48	40	43	-18	t
H38	24	48	44	43	-19	†
H39	22	48	39	43	-21	İ
H40	25	48	40	43	-18	İ
H41(BNAL02)	25	48	42	43	-18	
H42	24	48	48	43	-19	
H43	23	48	50	43	-20	
H44(BNAL14)	23	48	49	43	-20	
H45	22	48	39	43	-21	ł
H46 H47	23	48 48	40 46	43 43	-20 -19	<del> </del>
H48	23	48	42	43	-20	ł
H49	25	48	39	43	-18	†
H50	24	48	47	43	-19	İ
H51	24	48	46	43	-19	
H52	23	48	44	43	-20	
H53(BNAL16)	26	48	43	43	-17	
H54	25	48	39	43	-18	
H55	22	48	39	43	-21	
H56	25	48	41	43	-18	ł
H57 H58	25 18	48 48	41 36	43 43	-18 -25	†
H59	18	48	36	43	-25	t
H60	22	48	38	43	-21	İ
H61	19	48	38	43	-24	İ
H62	24	48	38	43	-19	
H63	18	48	37	43	-25	
H64	24	48	46	43	-19	1
H65	24	48	45	43	-19	ļ
H66	24	48	39	43	-19	+
H67	23	48	38	43	-20	<del> </del>
H68	24 24	48 48	39 39	43	-19 -19	<del> </del>
H69 H70	18	48 48	39	43 43	-19 -25	†
H71	23	48	40	43	-25 -20	t
H72	24	48	45	43	-19	†
H73	24	48	45	43	-19	İ
H74	22	48	39	43	-21	
H75	19	48	37	43	-24	I
H76	21	48	38	43	-22	Ţ
H77	25	48	42	43	-18	ļ
H78	25	48	42	43	-18	

H79     23     48     38     43       H80     24     48     43     43       H81     23     48     38     43       H82     21     48     37     43       H83     22     48     37     43       H84     20     48     37     43	-20 -19 -20
H81     23     48     38     43       H82     21     48     37     43       H83     22     48     37     43	-20
H82     21     48     37     43       H83     22     48     37     43	
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